



**FINNISH-JAPANESE WORKSHOP
ON FUNCTIONAL MATERIALS**
Espoo and Helsinki, Finland

May 25, 2009

Status of Photonics Polymers for “Fiber to the Display”

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Lightwave

?

**Polymer
Heterogeneous
Structure**

Correlation Length

Å
(10⁻¹⁰)

nm
(10⁻⁹)

μm
(10⁻⁶)

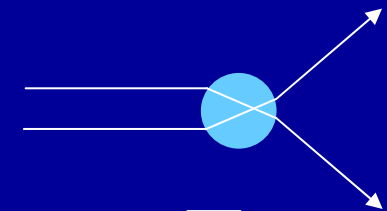
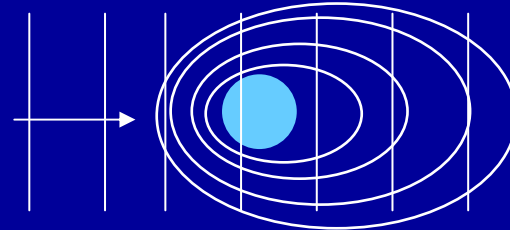
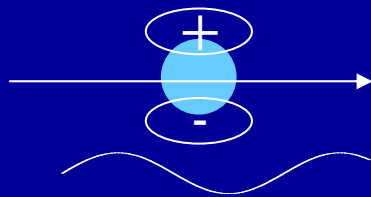
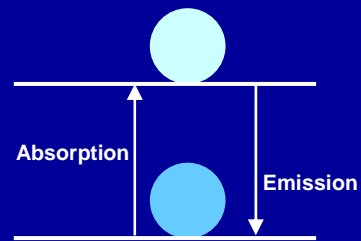
mm
(10⁻³)

Absorption
Emission

Polarization

Scattering

Refraction
Reflection



High-Power Optical Fiber
Amplifier and Laser

Zero-Birefringence
Polymer

Highly Scattering
Optical Transmission
(HSOT) Polymer

High Speed Graded-Index
Polymer Optical Fiber

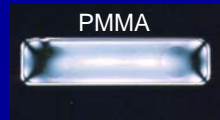
Eu Chelate-doped
polymer



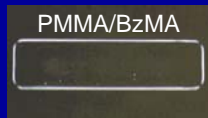
Ermine 6G-doped
polymer

Zero absorption Loss
Polymer

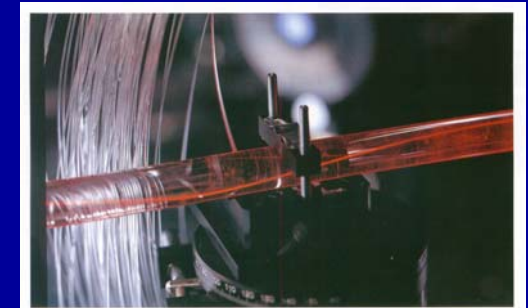
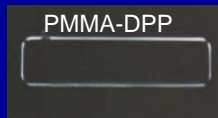
PMMA



PMMA/BzMA

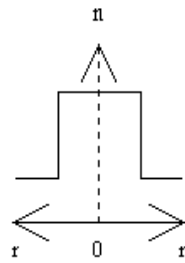


PMMA-DPP



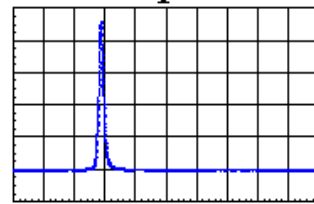


SIPOF

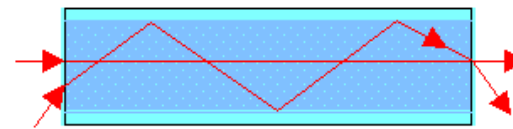


Cross Section

Input Pulse

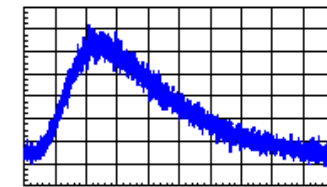


500ps/div



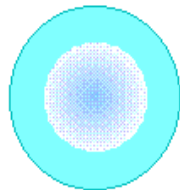
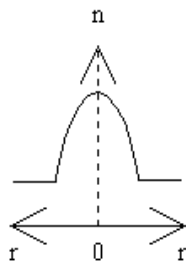
Ray Trajectory

Output Pulse after 100m Transmission



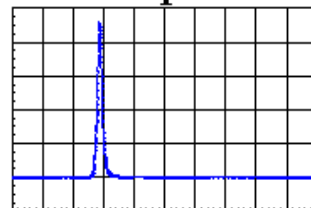
500ps/div

GIPOF

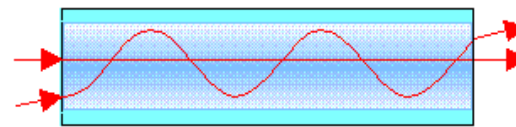


Cross Section

Input Pulse

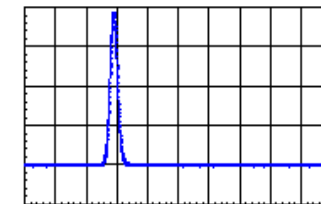


500ps/div



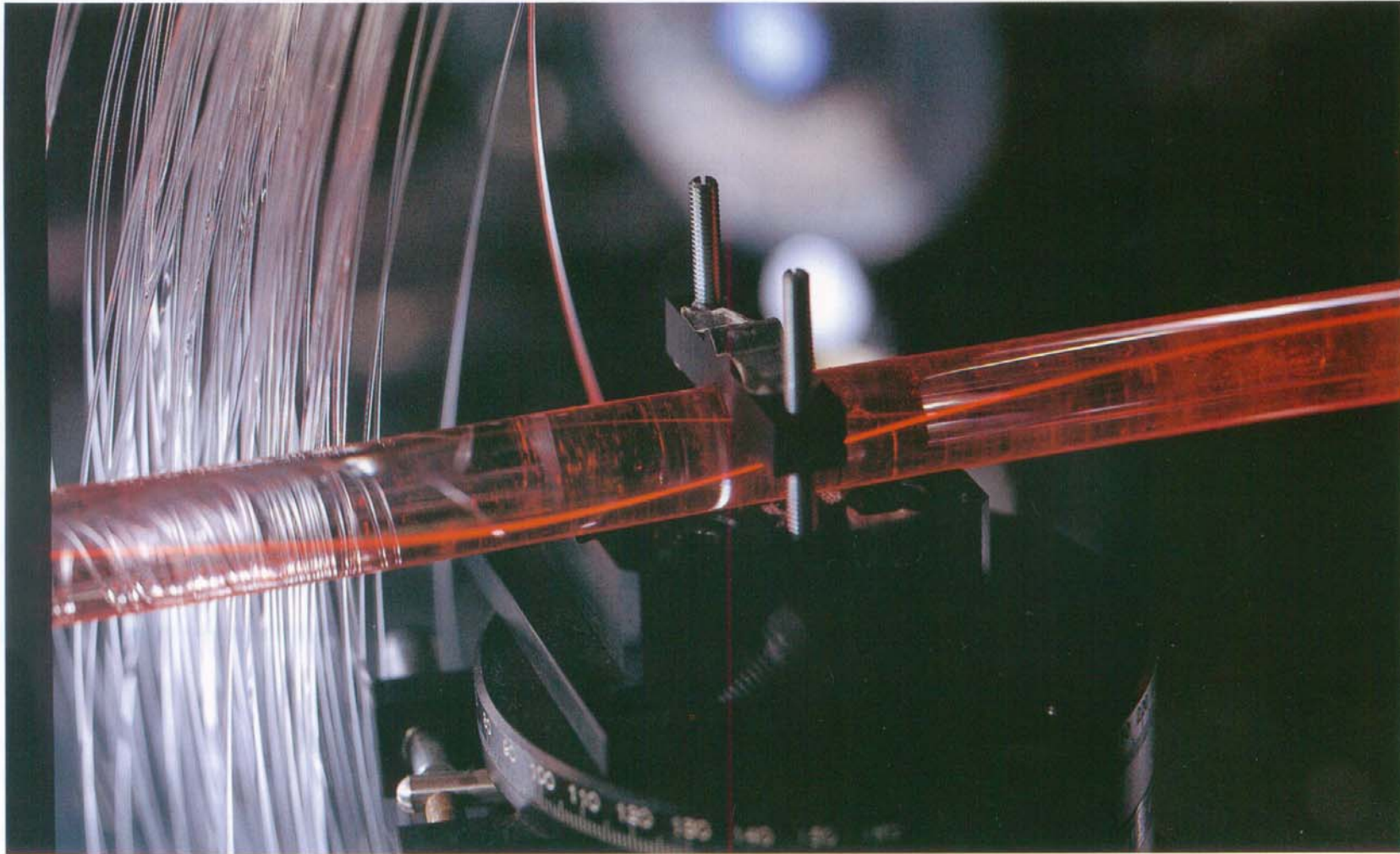
Ray Trajectory

Output Pulse after 100m Transmission

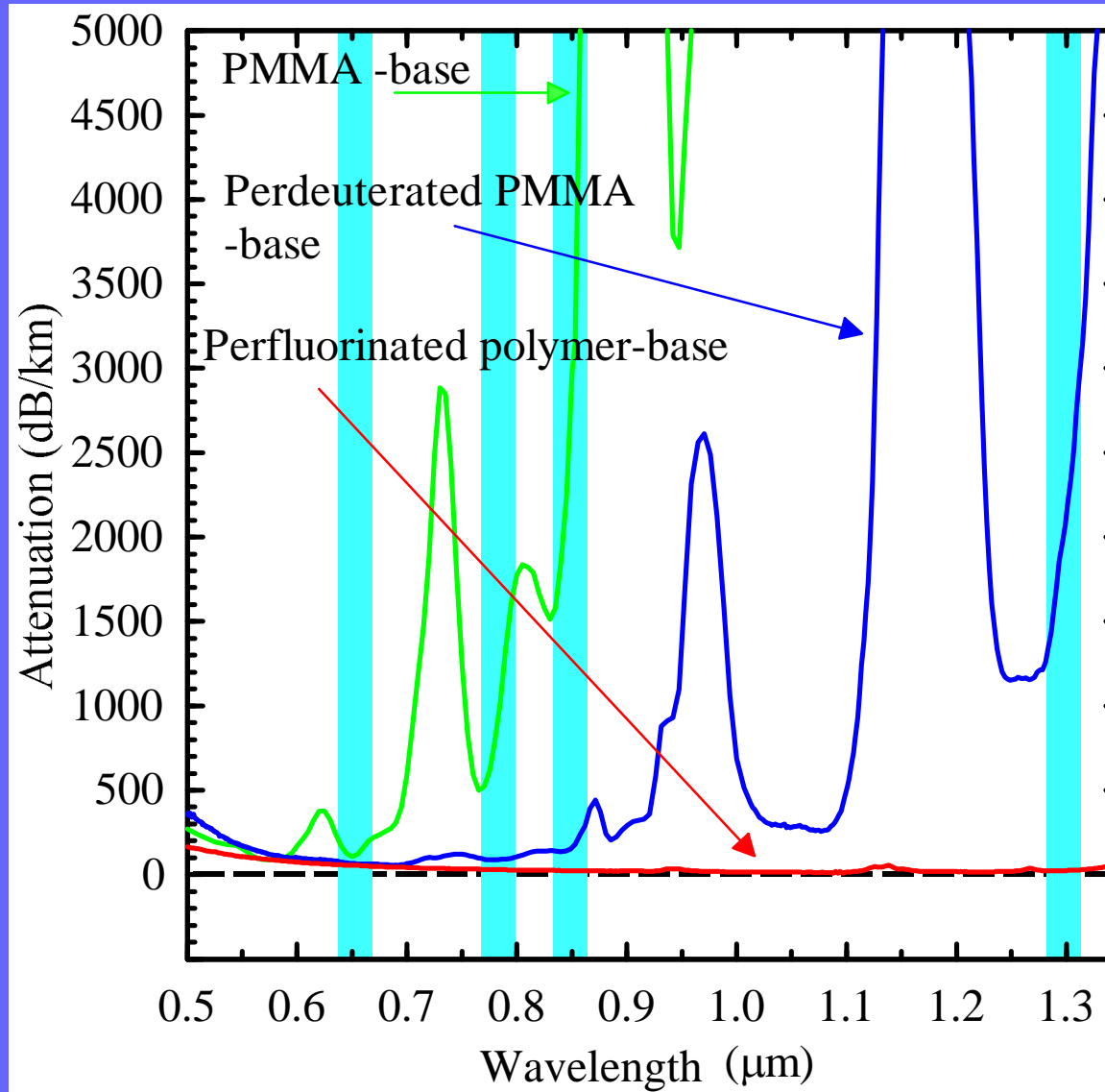


500ps/div

Comparison of Step-Index Plastic Optical Fiber (SIPOF) and Graded-Index Plastic Optical Fiber (GI-POF).



High-Speed GI Plastic Optical Fiber

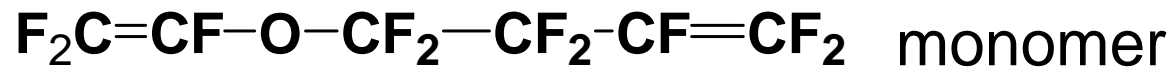
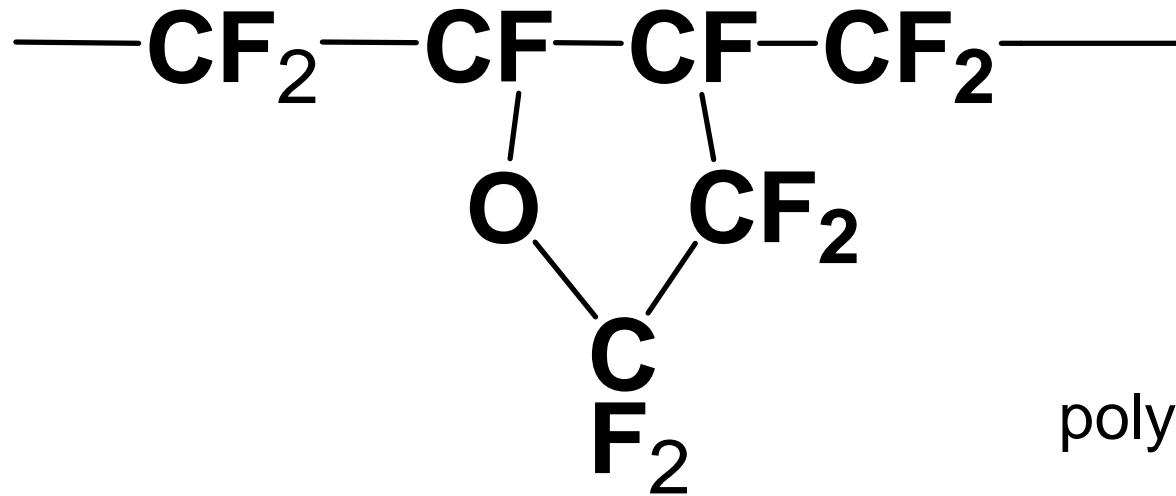


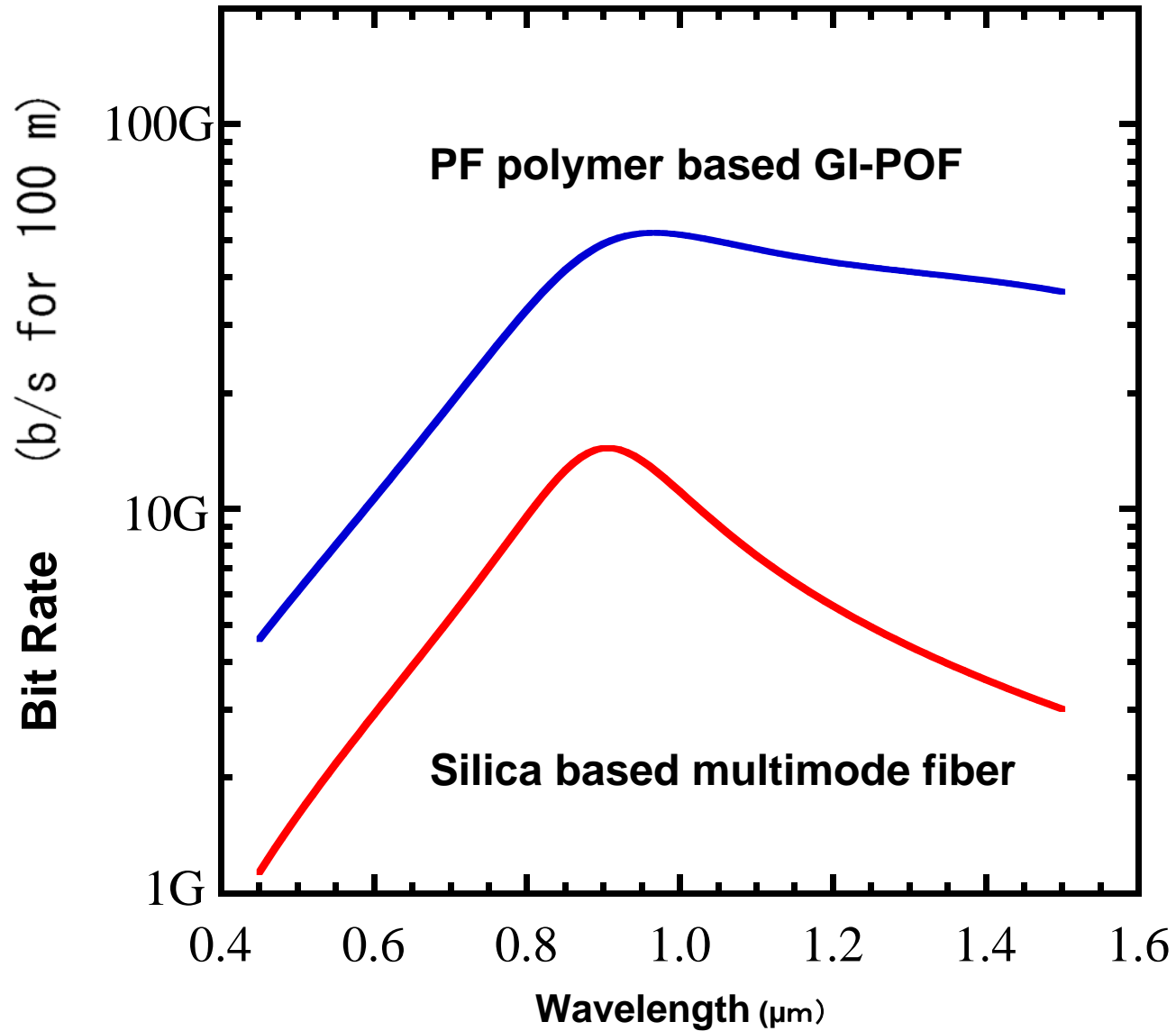
Total Attenuation Spectra of GI POFs.

CYTOP(Perfluoro butenyl vinyl ether) -Asahi Glass Co.-

The material for commercial GI-POF (Lucina)

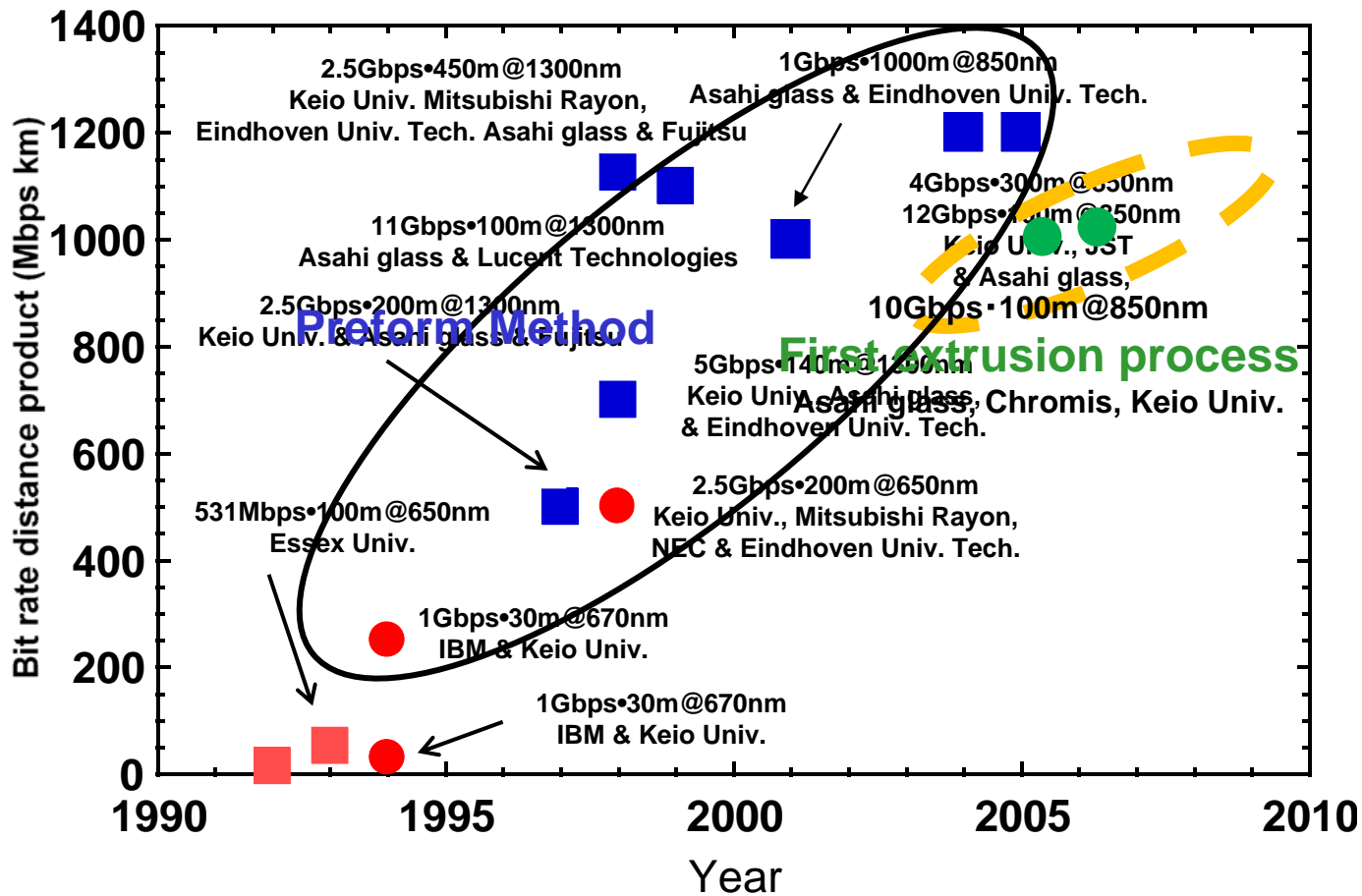
Tg: ~108°C





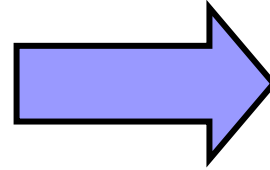
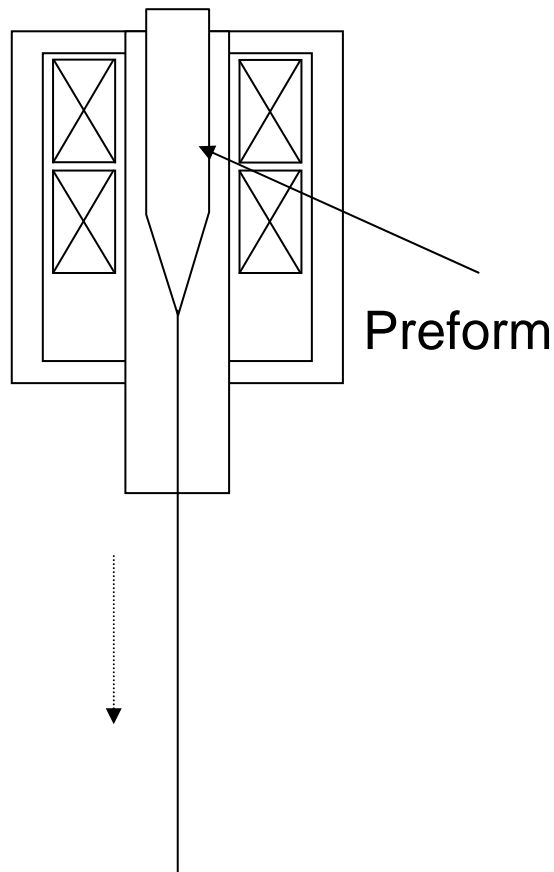
Calculated bandwidth potential of PF polymer based GI-POF compared with that of silica based MMF.

Development of data rate achieved by POF links

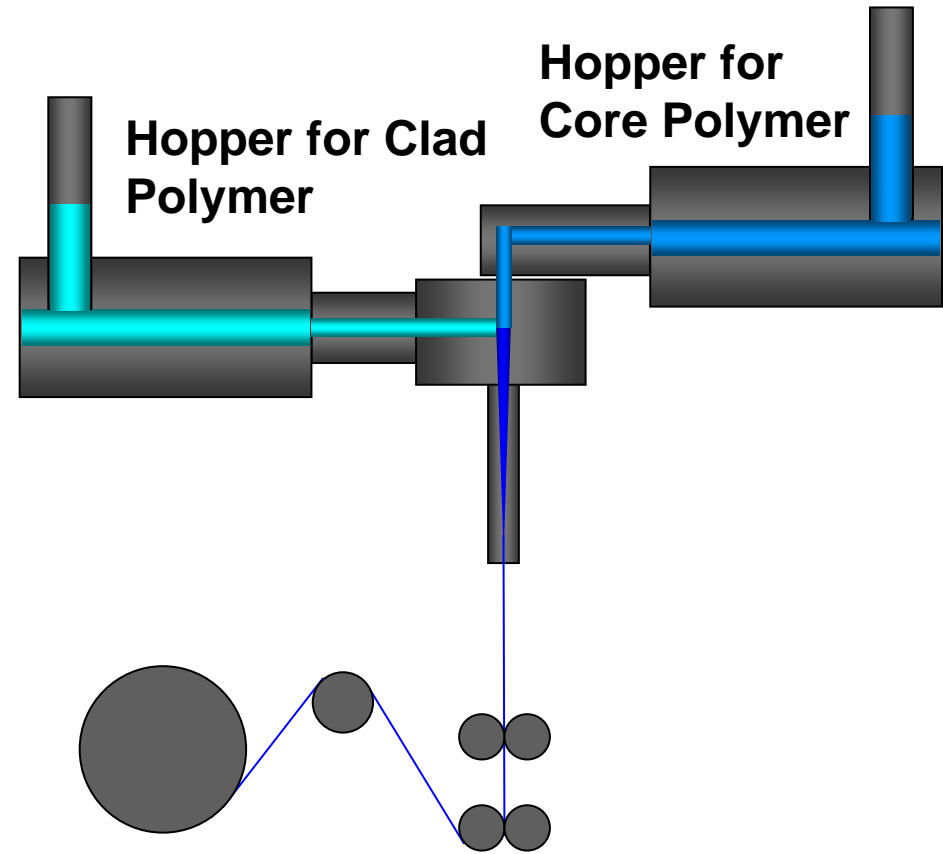


R&D Project of Polymer Devices for Constructing Next-Generation FTTH (METI, 2004-2006)

Preform Method



Extrusion Process

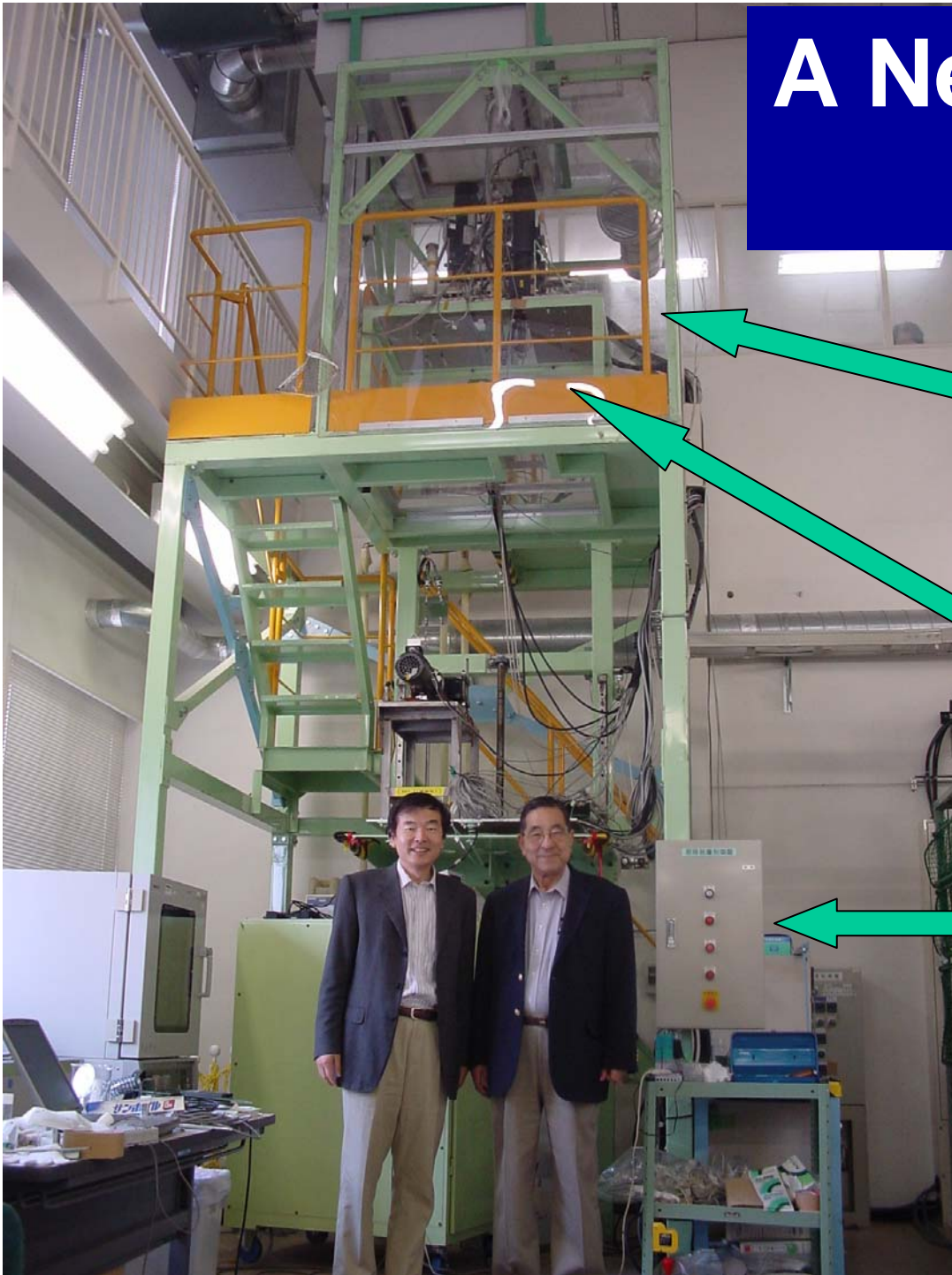


A New Co-Extrusion Tower

Hopper for Core and Clad Polymer

Diffusion Zone

Control Panel



Correlation Length

Å
(10⁻¹⁰)

nm
(10⁻⁹)

μm
(10⁻⁶)

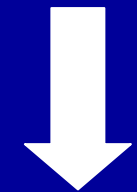
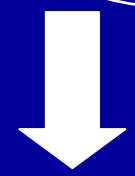
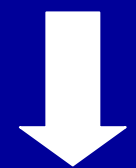
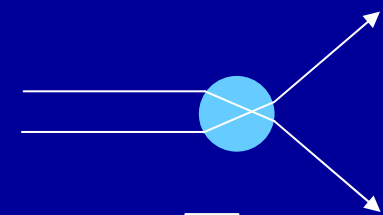
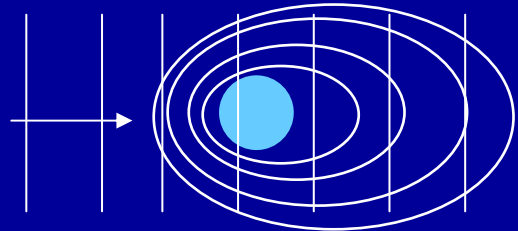
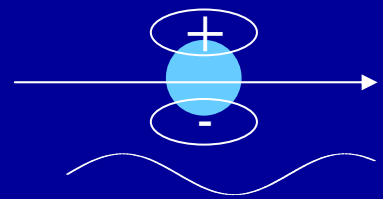
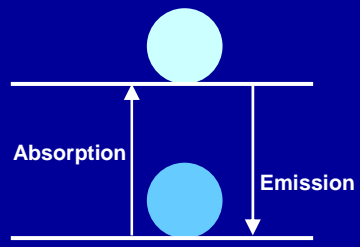
mm
(10⁻³)

Absorption
Emission

Polarization

Scattering

Refraction
Reflection

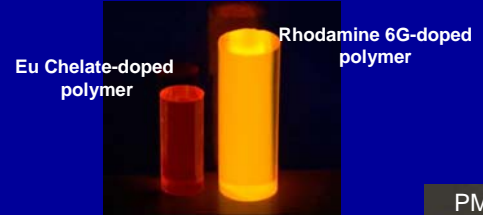


High-Power Optical Fiber
Amplifier and Laser

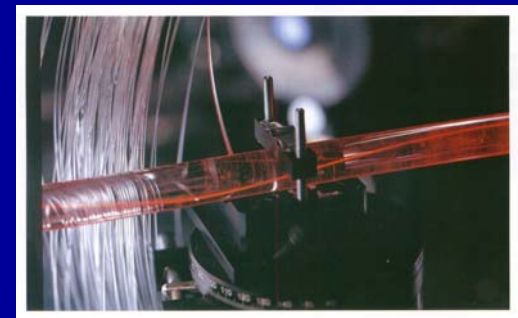
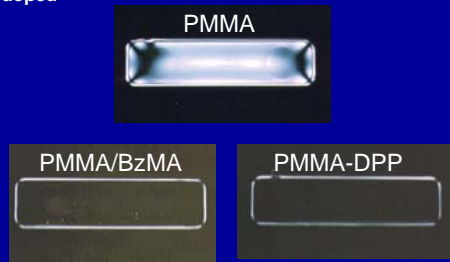
Zero-Birefringence
Polymer

Highly Scattering
Optical Transmission
(HSOT) Polymer

High Speed Graded-Index
Polymer Optical Fiber



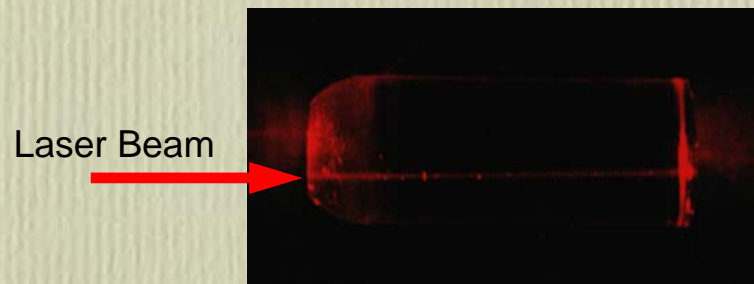
Zero absorption Loss
Polymer



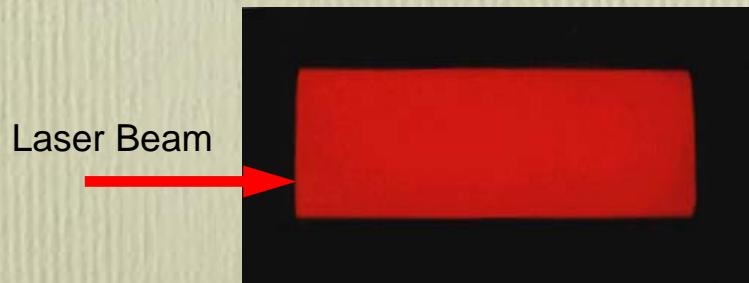
Proposal of Highly Scattered Optical Transmission (HSOT) Polymer



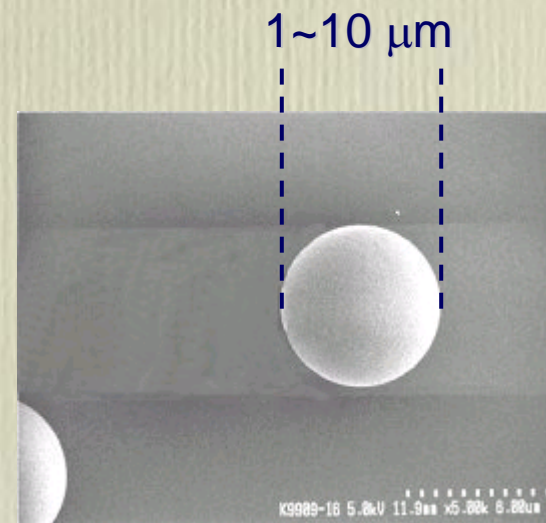
Highly Scattering Optical Transmission (HSOT) Polymer



(A) PMMA

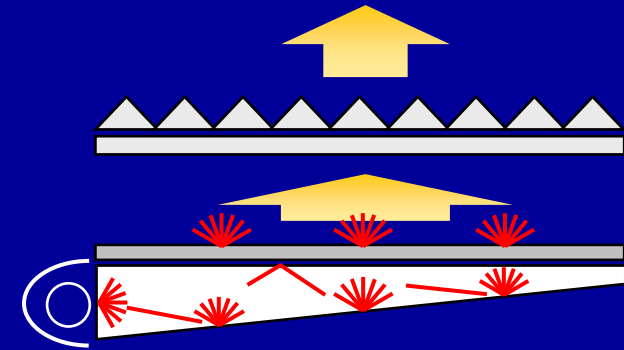
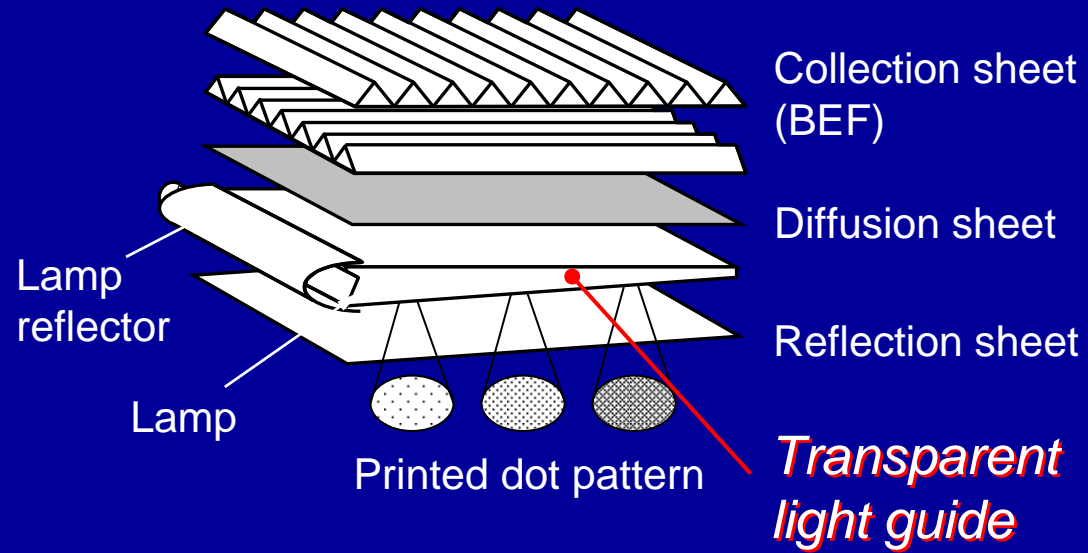


(B) HSOT polymer

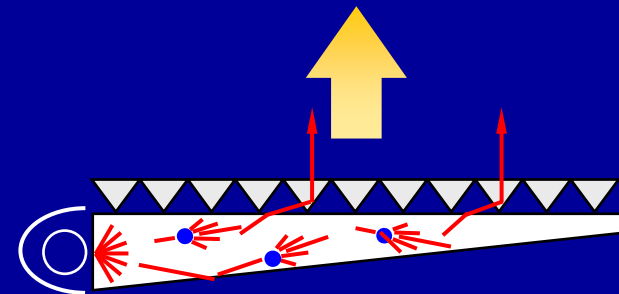
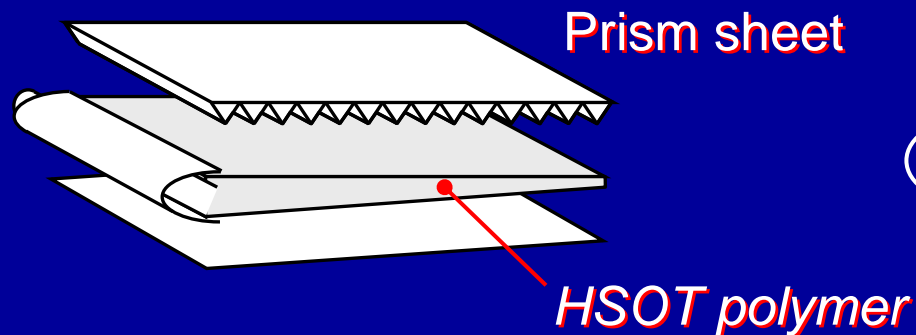


(FIG.1.1, p.11)

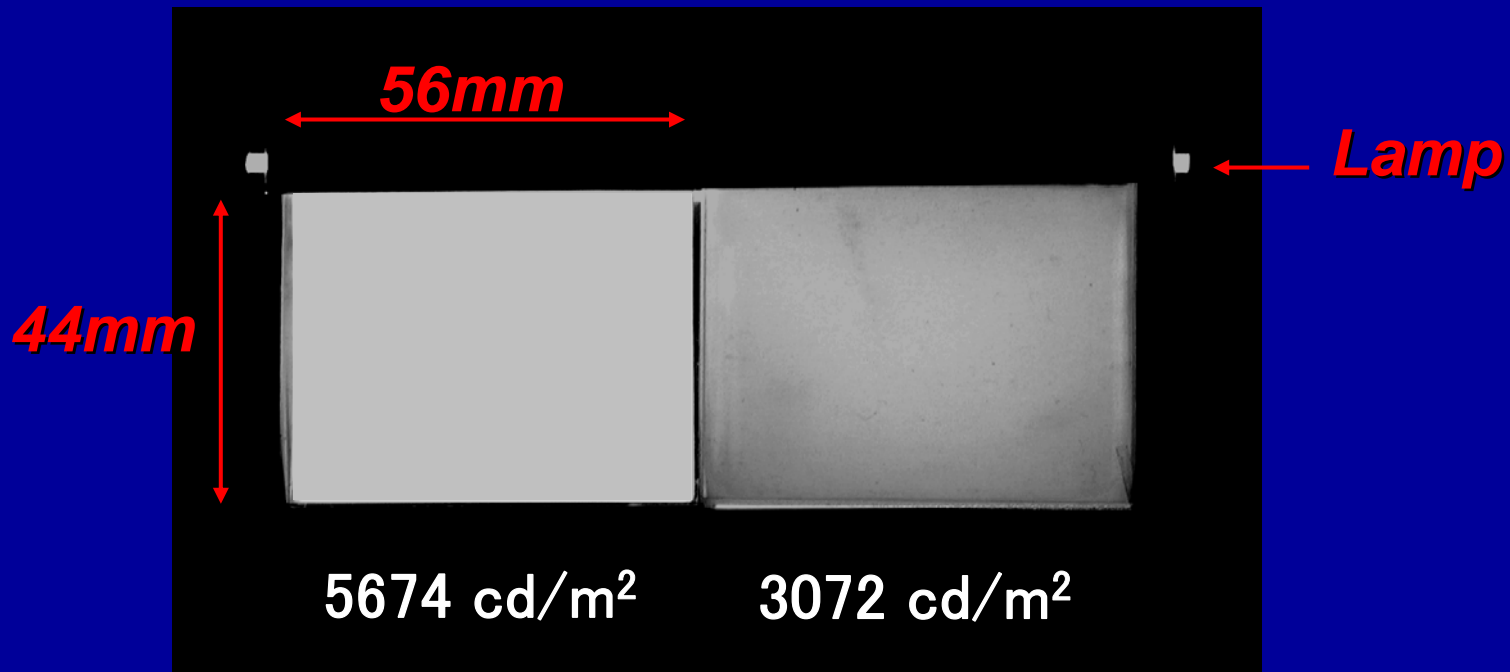
(A) Conventional backlighting system



(B) HSOT backlighting system



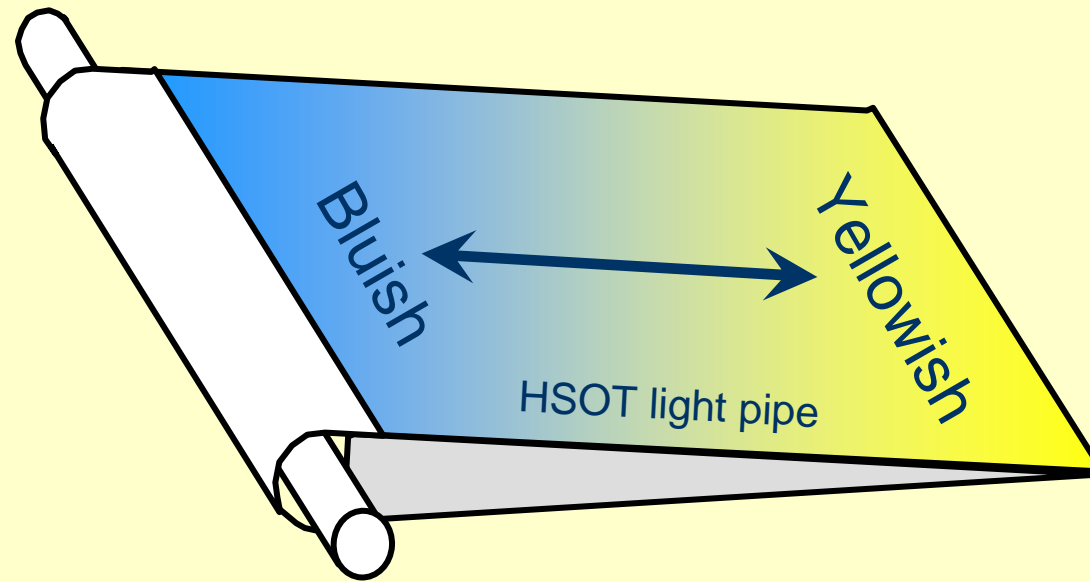
HSOT and conventional backlights



*HSOT
backlight*

*Conventional
backlight*

Is General Concept of Light Scattering Always True?



Color dispersion due to general light scattering phenomenon

Photograph of Sunset



Mie scattering theory

$$I(\alpha, \theta) = \lambda^2 (i_1 + i_2) / 8\pi^2$$

$$K(\alpha) = \frac{2}{\alpha^2} \sum_{n=1}^{\infty} (2n+1) (|a_n|^2 + |b_n|^2)$$

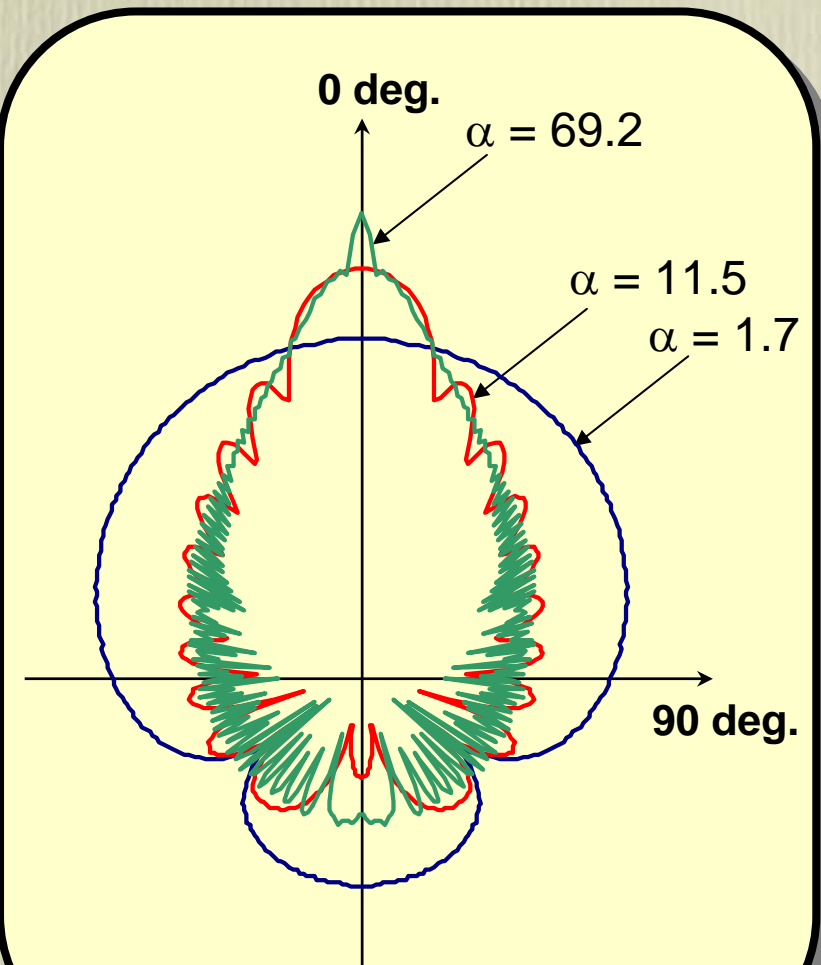
$$a_n = \frac{\psi_n(\alpha)\psi_n'(m\alpha) - m\psi_n(m\alpha)\psi_n'(\alpha)}{\zeta_n(\alpha)\psi_n'(m\alpha) - m\psi_n(m\alpha)\zeta_n'(\alpha)}$$

$$b_n = \frac{m\psi_n(\alpha)\psi_n'(m\alpha) - \psi_n(m\alpha)\psi_n'(\alpha)}{m\zeta_n(\alpha)\psi_n'(m\alpha) - \psi_n(m\alpha)\zeta_n'(\alpha)}$$

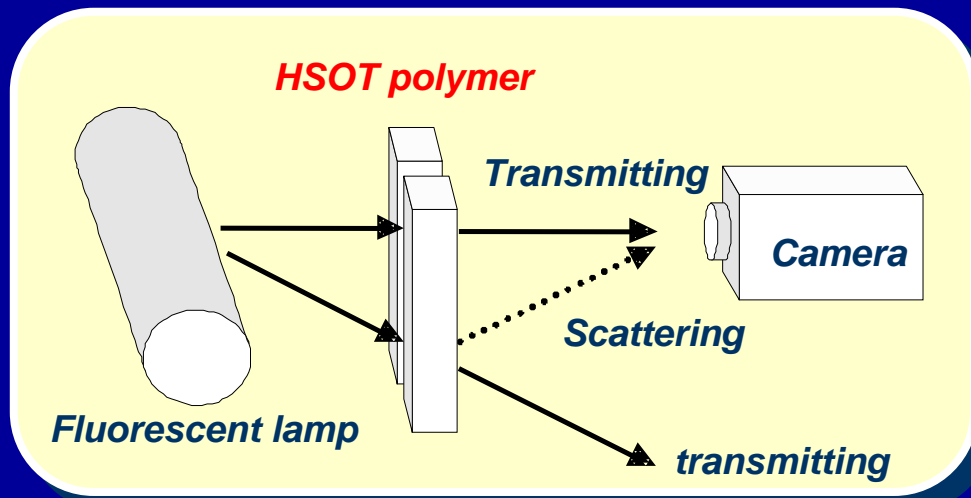
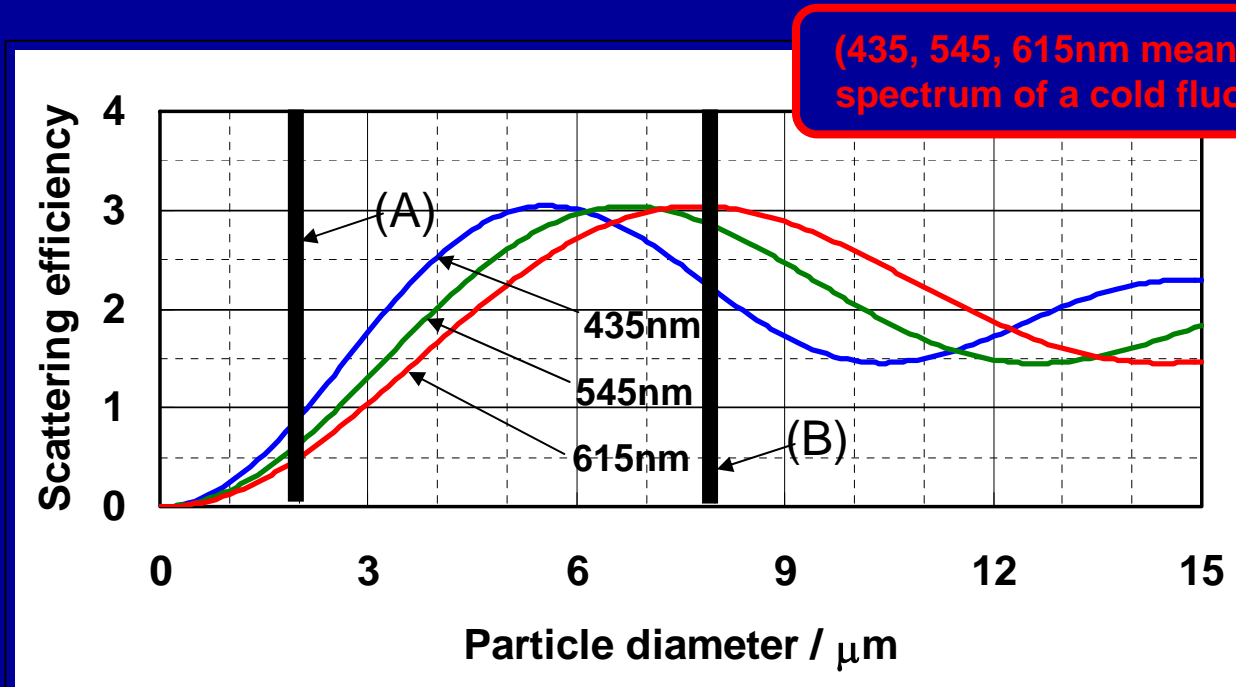
$$i_1 = \left[\sum_{n=1}^{\infty} \frac{2n+1}{n(n+1)} \left\{ a_n \frac{P_n^{(1)}(\cos\theta)}{\sin\theta} + b_n \frac{dP_n^{(1)}(\cos\theta)}{d\theta} \right\} \right]^2$$

$$i_2 = \left[\sum_{n=1}^{\infty} \frac{2n+1}{n(n+1)} \left\{ b_n \frac{P_n^{(1)}(\cos\theta)}{\sin\theta} + a_n \frac{dP_n^{(1)}(\cos\theta)}{d\theta} \right\} \right]^2$$

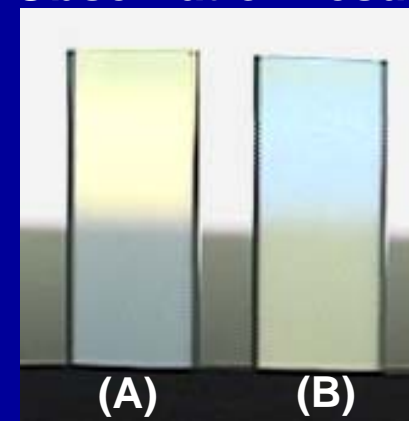
$$\alpha = 2\pi r / \lambda$$



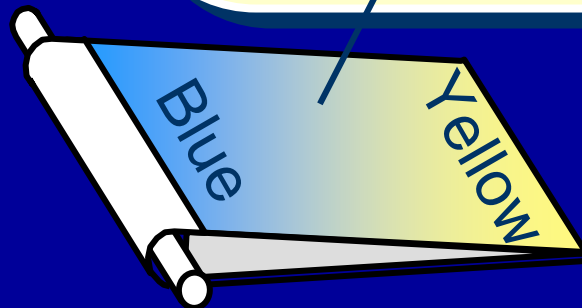
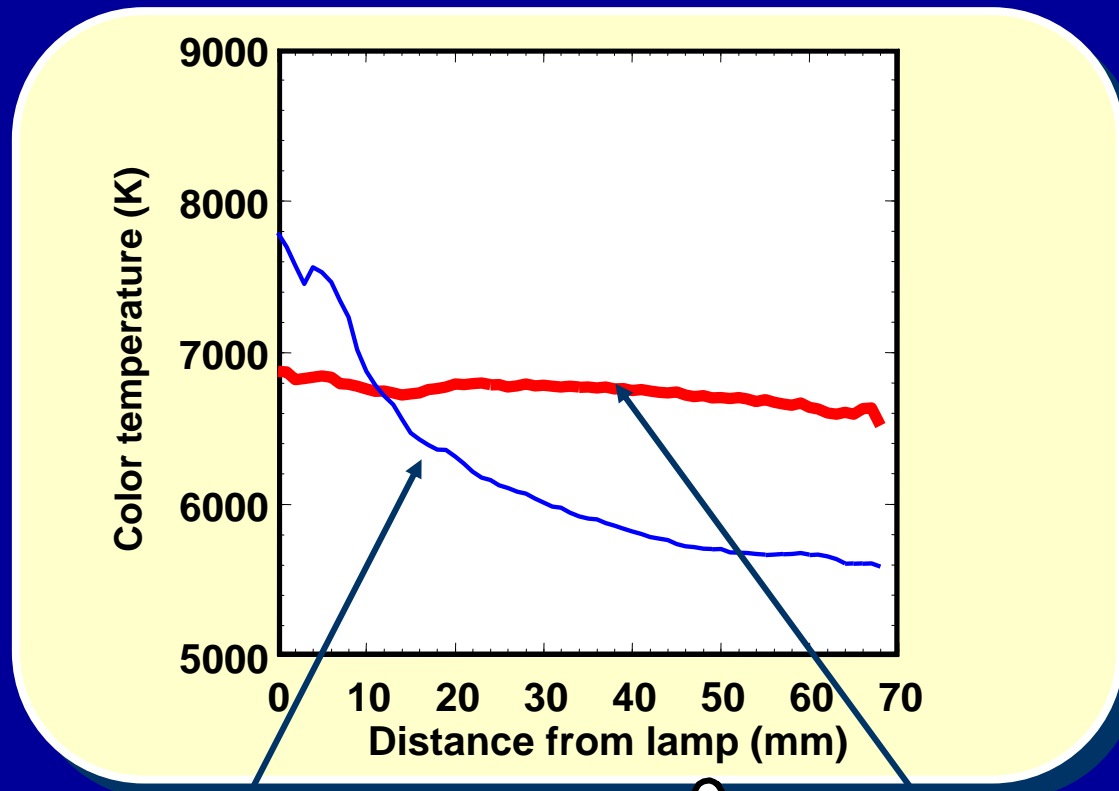
Scattering Efficiency



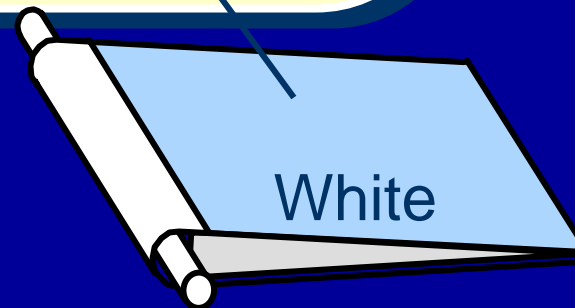
Observation result



Color Dispersion on HSOT Backlights



Not optimized HSOT



Optimized HSOT

HSOT Polymer Products



Notebook PCs

SONY Vaio Note series
Panasonic Let's Note series
TOSHIBA Dynabook series
Samsung, Dell etc.



Various Mobile Devices

Mobile phones
PDA
Pocket TV

Light Guide for LCD-TV

FUJIFILM
Light Guide for LCD TV
Flexible extremely thin and light large screen LCD TVs
Highly efficient light source

Technology
• Surface Design Technology
• Light Scattering Particle Technology

Concept
"SILICON" Stage of LCD-TV in the Future!
- Light Scattering Types for Multi-applications



Evolution of Backlight LCD-TV



57 inch LCD Module

Display	Backlighting
Technology	LED
Resolution	1920 x 1080
Weight	10.5kg
Thickness	10.5mm
Power Consumption	100W


Do NOT Touch!

FUJIFILM
Novel Transparent Conductive Film
New technology combined with the Shield Rex film for PDP

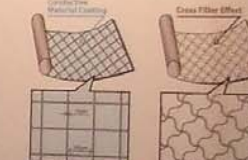
Features

- 1.Ultra High Conductivity: Surface resistance 0.3Ω/□
- 2.High Flexibility: Stable conductivity even after repeated bending (4mmφ, bend test 100 times.)
- 3.High Transparency: Transparency over 80%.
- 4.Seamless Pattern: Seamless/Continuous fine conductive line pattern

Current Shield Rex Film



New Film



FUJIFILM

Correlation Length

Å
(10⁻¹⁰)

nm
(10⁻⁹)

μm
(10⁻⁶)

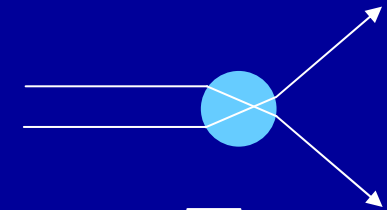
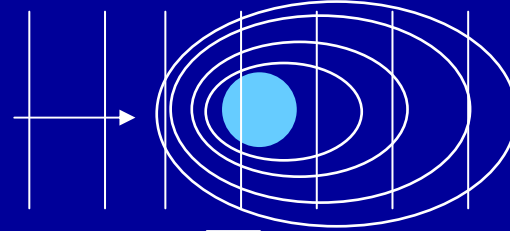
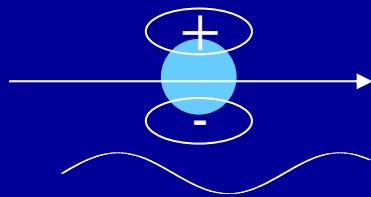
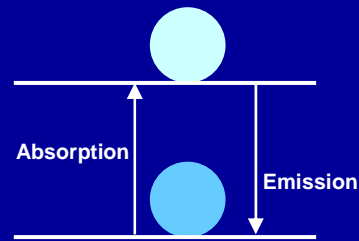
mm
(10⁻³)

Absorption
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High-Power Optical Fiber
Amplifier and Laser

Zero-Birefringence
Polymer

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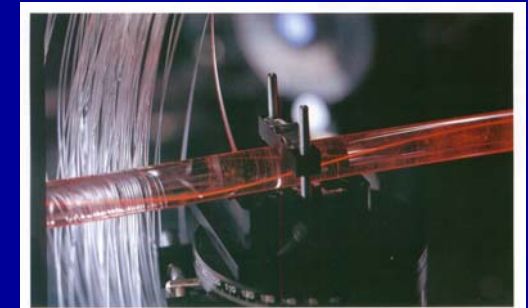
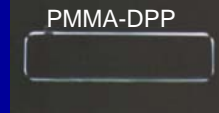
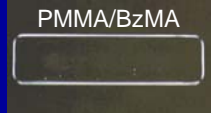
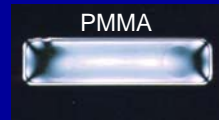
High Speed Graded-Index
Polymer Optical Fiber

Eu Chelate-doped
polymer



Zero absorption Loss
Polymer

Rhodamine 6G-doped
polymer

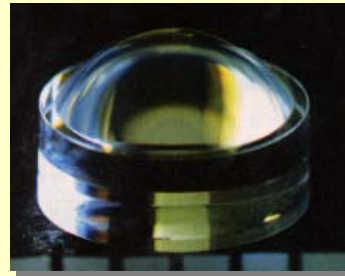


Advantage of zero-birefringence optical polymers

Flexibility
Light weight
Low cost



Birefringence



- Solvent Casting ··· Low birefringence, **High cost.**

Zero-birefringence polymers

- Extrusion processing ··· High speed, Low cost and zero-birefringence.

Changing in polarization state through a birefringent medium

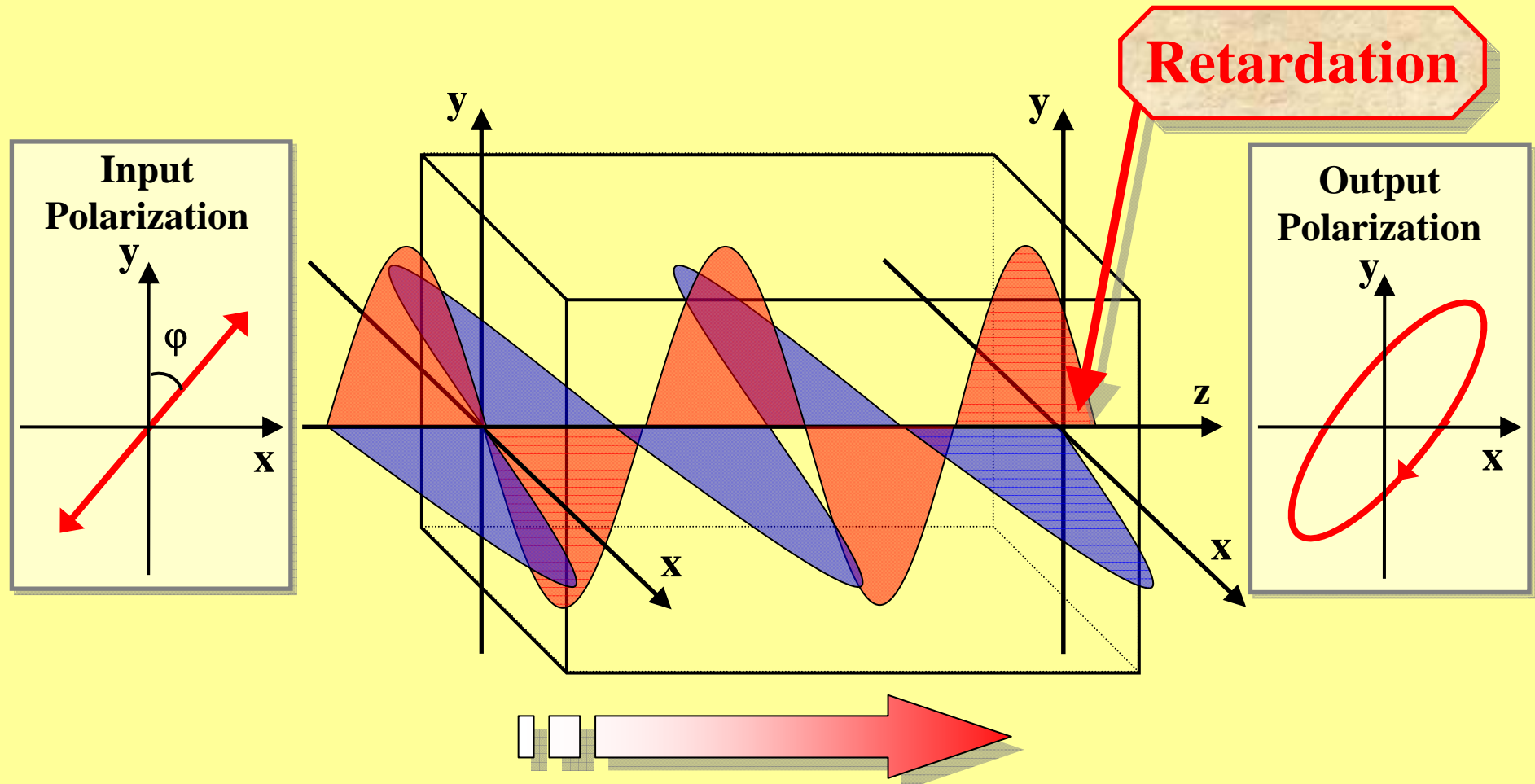


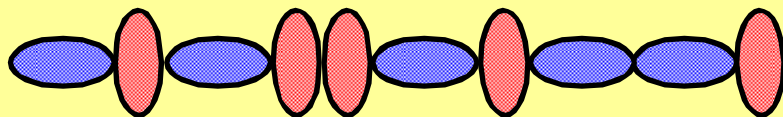
Figure Polarization property in a birefringent medium.

Our proposal of compensating orientational birefringence of polymers

Random copolymerization method

Positive (+) birefringence monomer
Negative(-) birefringence monomer

Random
copolymerization



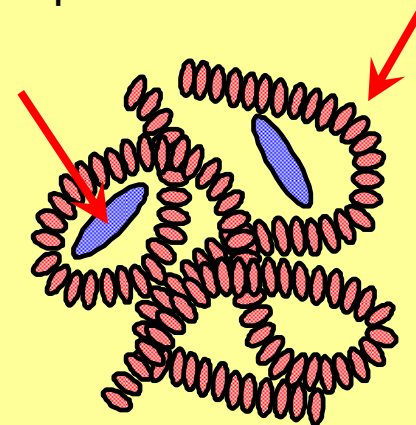
Zero-birefringence copolymer

MMA / BzMA = 82 / 18 (wt./wt.)

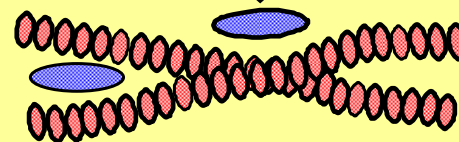
Anisotropic molecule dopant method

Polarizability ellipsoid
of anisotropic
molecule

Polarizability ellipsoid
of monomer unit

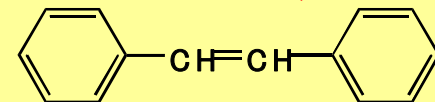


Drawing

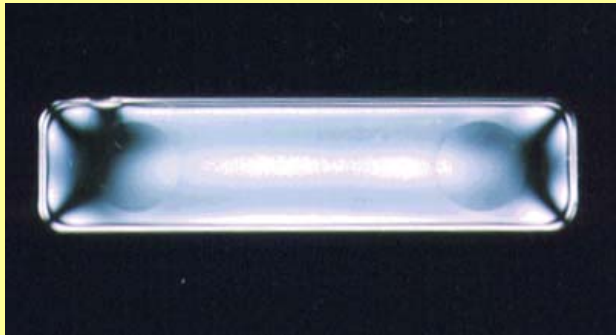


MMA / *trans*-stilbene = 100 / 3 (wt./wt.)

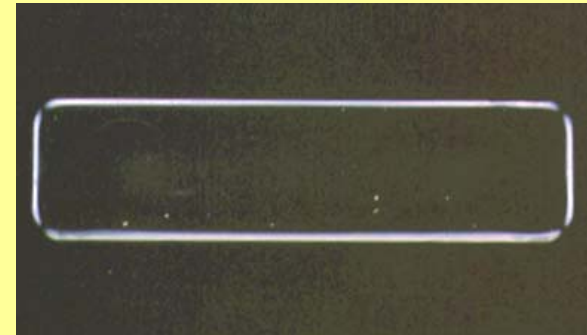
Typical dopant



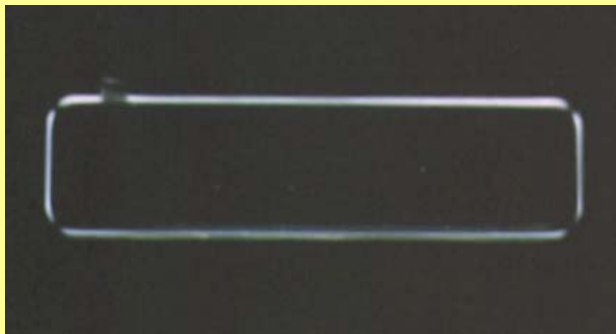
Injection molded samples



(a) PMMA

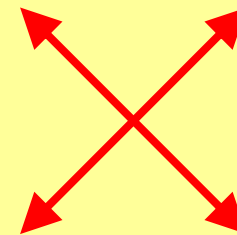


(b) MMA/BzMA=82/18 (wt./wt.)

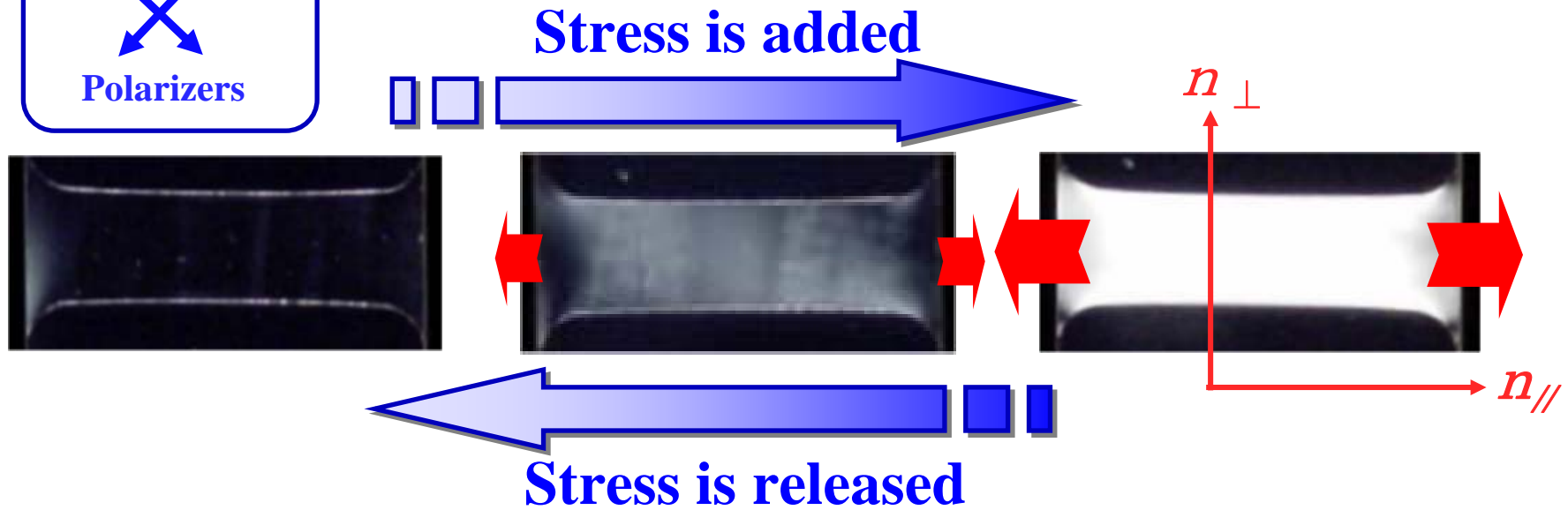


(c) PMMA-*trans*-stilbene (3 wt.%)

polarizer analyzer



Photoelastic Birefringence

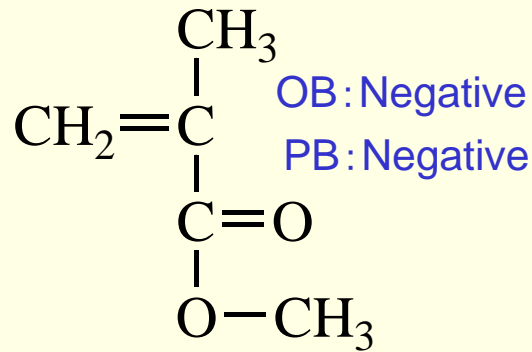


$$\Delta n = n_{\parallel} - n_{\perp} = c \cdot \Delta \sigma$$

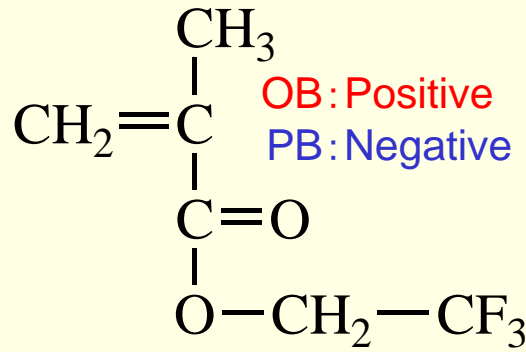
c : Photoelastic Coefficient
 $\Delta \sigma$: Stress

Components of Zero-Zero Polymers

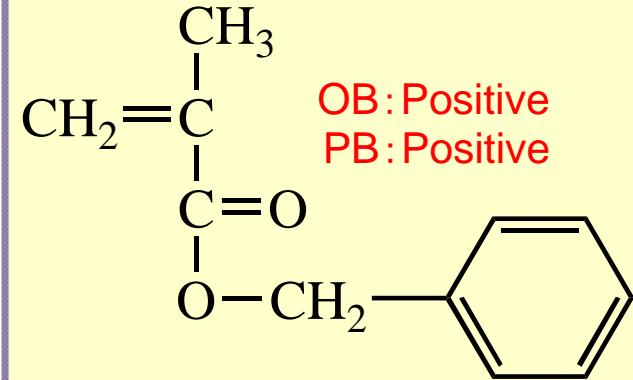
Monomers



Methyl methacrylate
(MMA)

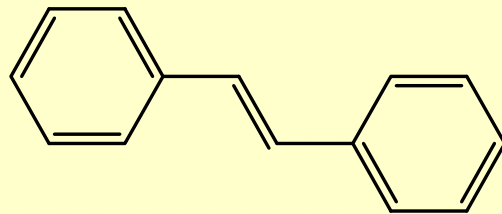


2,2,2-Trifluoroethyl
methacrylate (3FMA)



Benzyl methacrylate
(BzMA)

Anisotropic Dopant



trans-stilbene

OB: Positive
PB: Positive

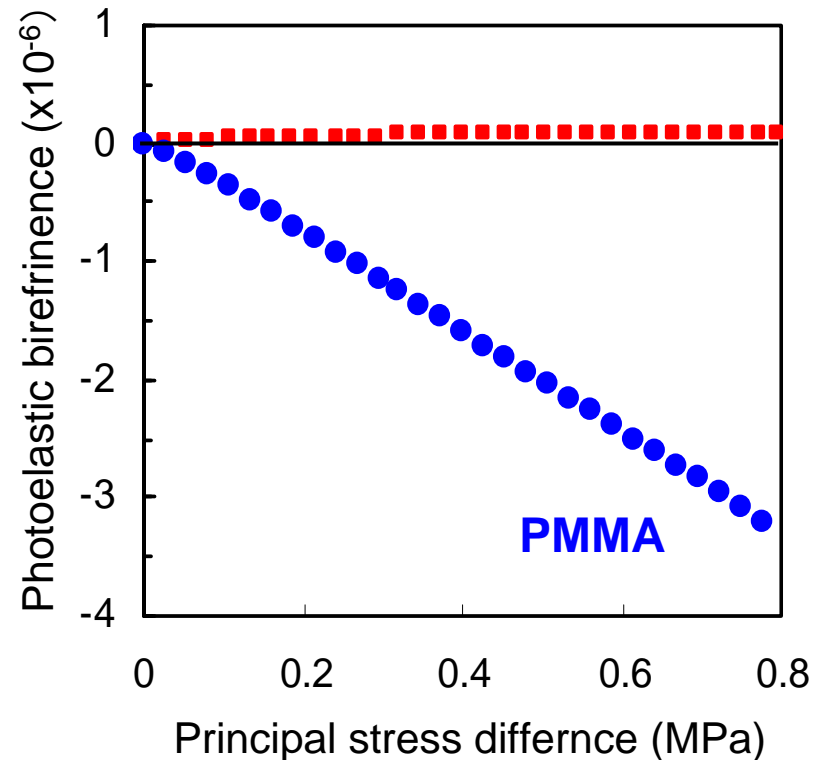
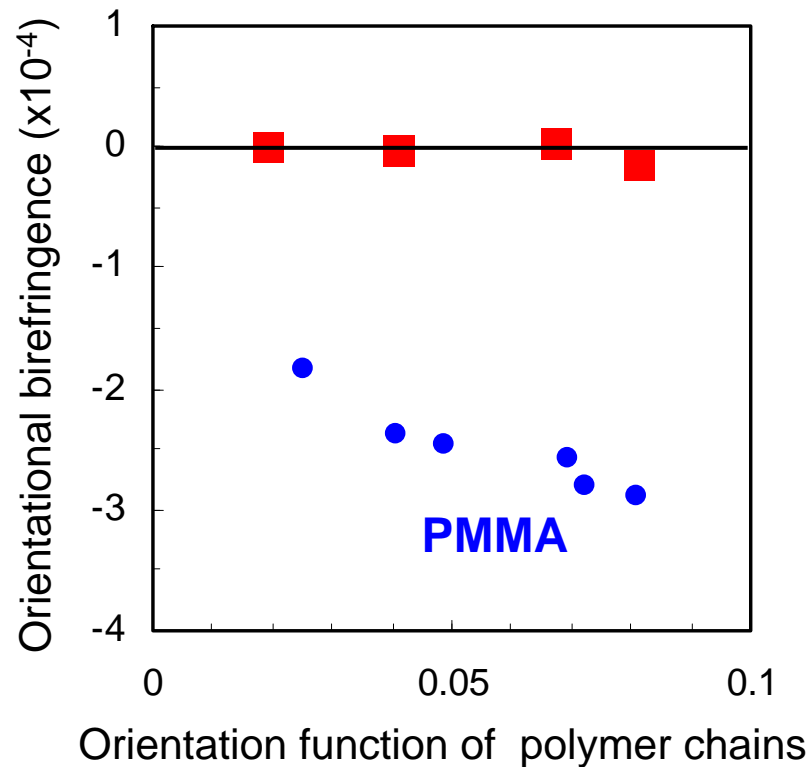
Ternary Copolymers

OB: Orientational Birefringence
PB: Photoelastic Birefringence

Binary Copolymers Containing an Anisotropic Dopant

Birefringence of Binary Copolymers Containing an Anisotropic Dopant

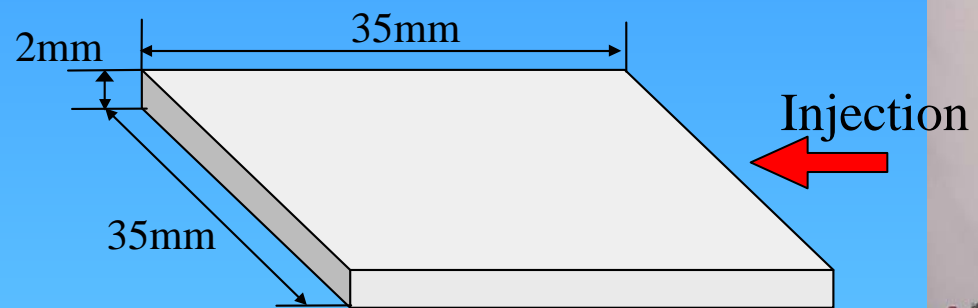
Simultaneous elimination of the orientational birefringence and photoelastic birefringence was achieved. Zero-zero polymers that exhibit no birefringence with any orientation of the polymer main chains and in elastic deformation was realized.



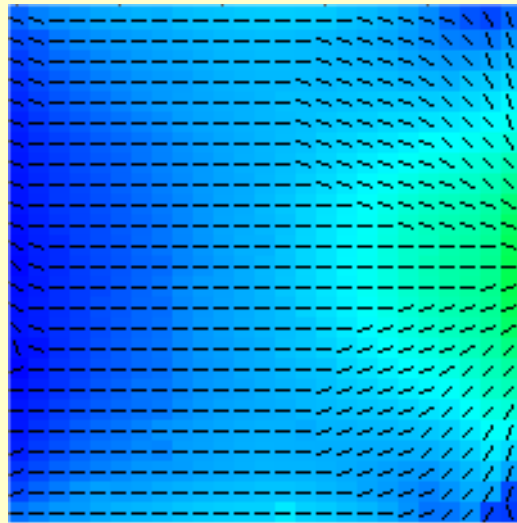
Composition of the zero-zero polymer

P(MMA/3FMA=85/15) + *trans*-stilbene 2.8 wt%

Injection Molding

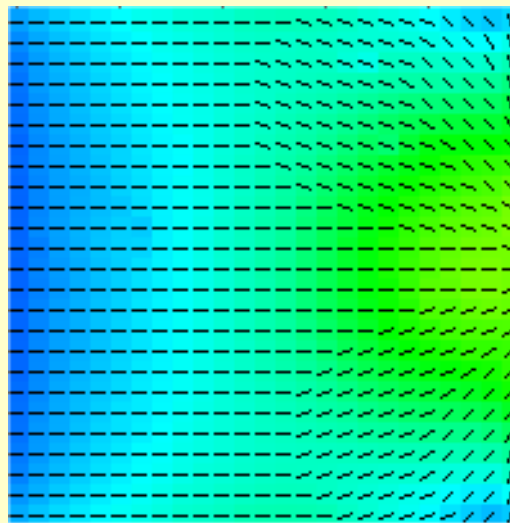


Injection Molded Samples of Binary Copolymer



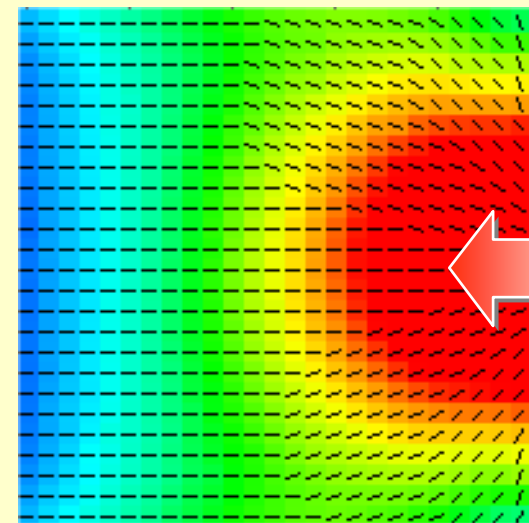
(a) 230 °C

$Re_{ave} = 2.4$ (nm)



(b) 220 °C

$Re_{ave} = 4.7$ (nm)



(c) 210 °C

$Re_{ave} = 9.1$ (nm)

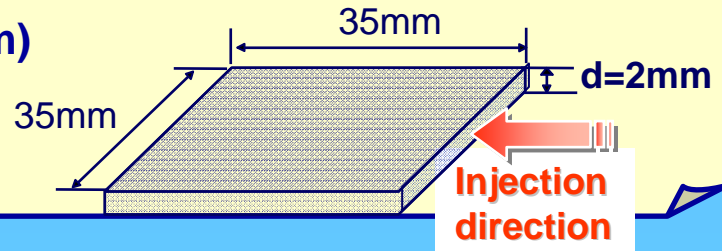


0 7.5 15

Re (nm)

$$Re = \Delta n \times d (= 2\text{mm})$$

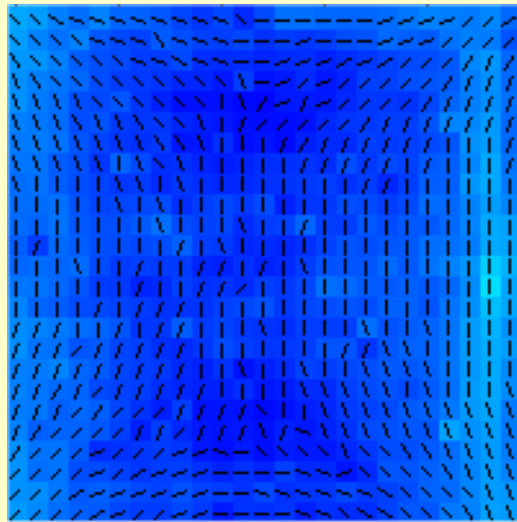
/, \, -, | : Fast axes



P(MMA/BzMA = 92/8)

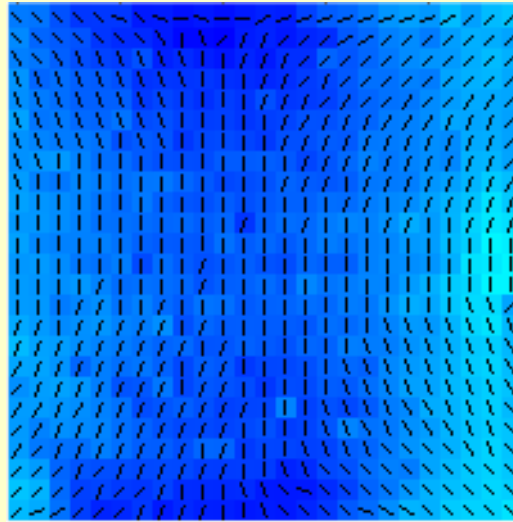
Orientational birefringence increased with a decrease in molding temperature. The directions of fast axes were parallel to injection direction.

Injection Molded Samples of the Ternary Copolymer



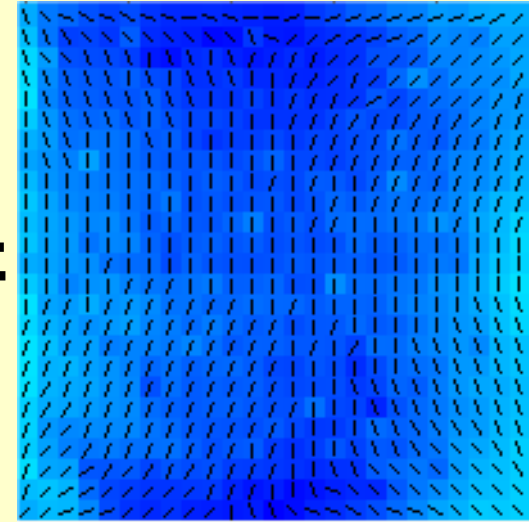
(a) 230 °C

$Re_{ave} = 0.4$ (nm)



(b) 210 °C

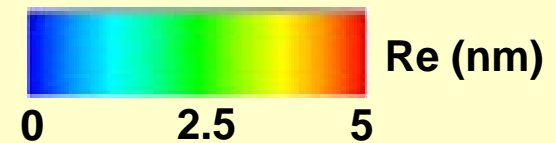
$Re_{ave} = 0.5$ (nm)



(c) 190 °C

$Re_{ave} = 0.5$ (nm)

/, \, —, | : Fast axes



P(MMA/3FMA/BzMA = 52/42/6)

Ternary copolymer exhibited close to zero birefringence at any points regardless of molding temperature.

Correlation Length

Å
(10⁻¹⁰)

nm
(10⁻⁹)

μm
(10⁻⁶)

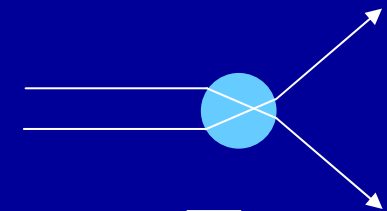
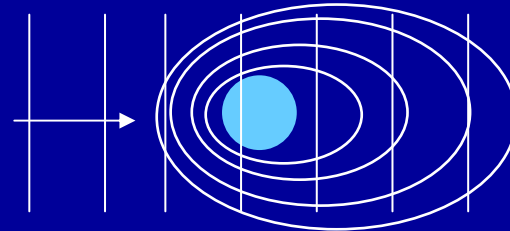
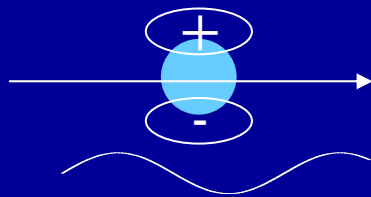
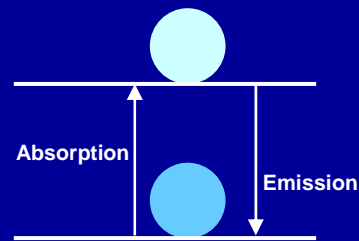
mm
(10⁻³)

Absorption
Emission

Polarization

Scattering

Refraction
Reflection



High-Power Optical Fiber
Amplifier and Laser

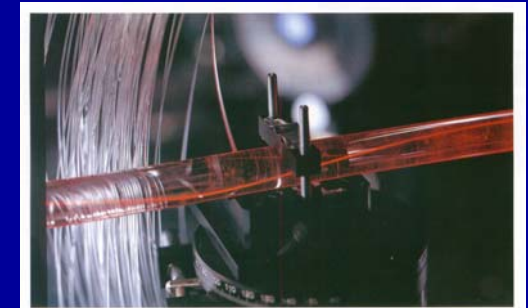
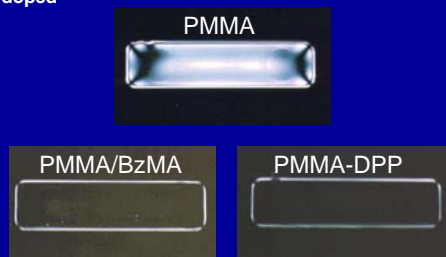
Zero-Birefringence
Polymer

Highly Scattering
Optical Transmission
(HSOT) Polymer

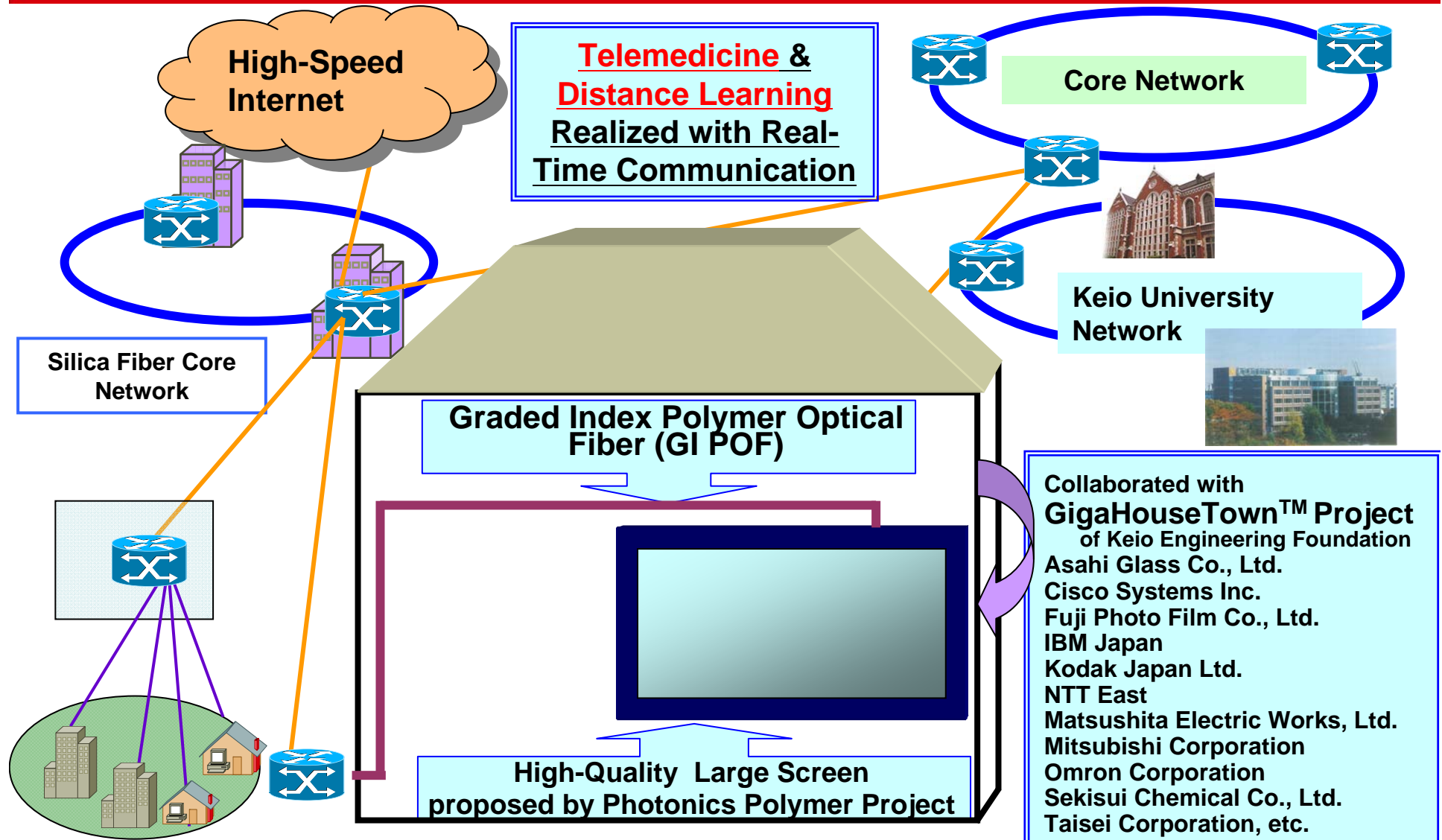
High Speed Graded-Index
Polymer Optical Fiber



Zero absorption Loss
Polymer

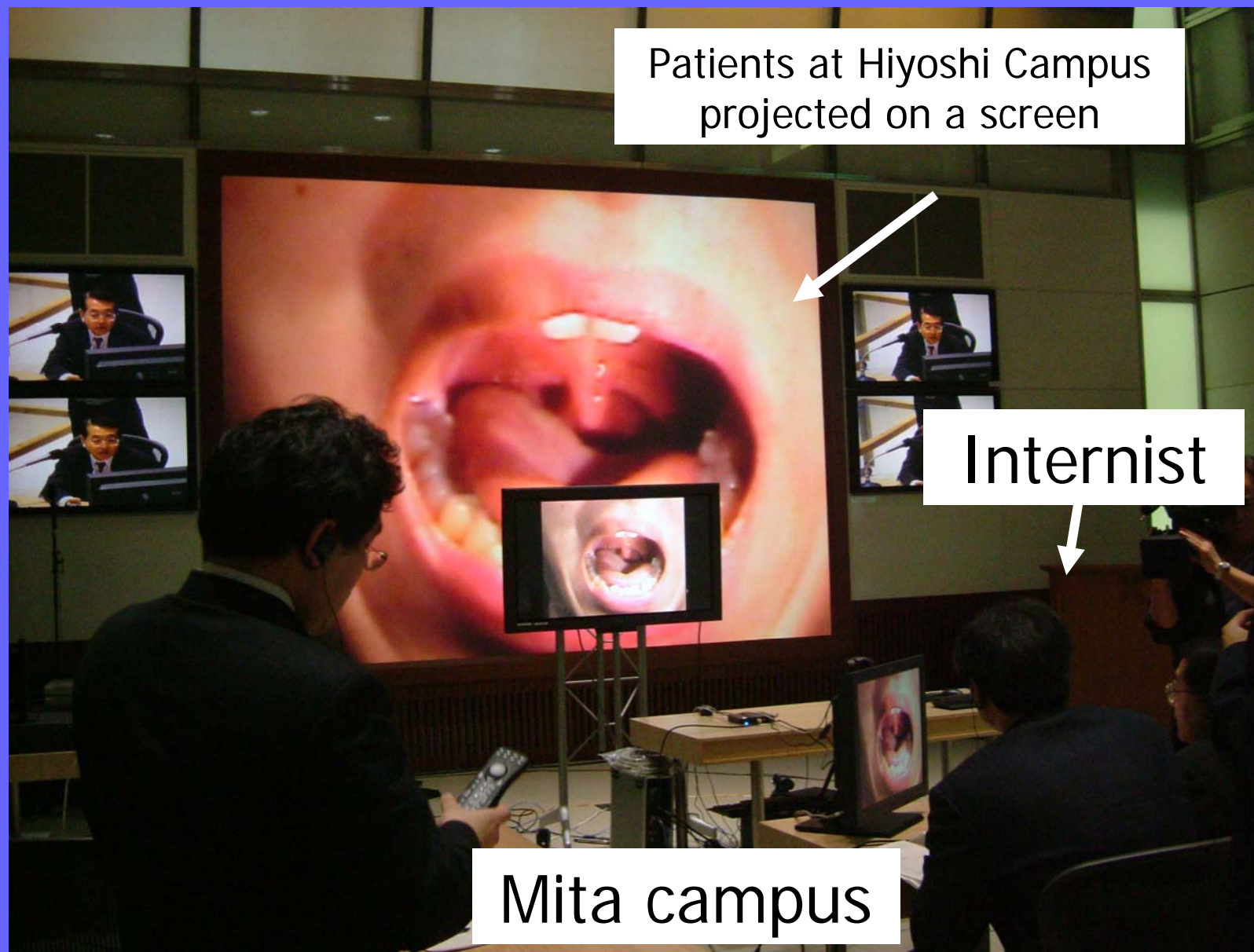


Photonics Polymer Project



Concept of "Fiber-to-the-Display" by Photonics Polymer Project at Keio University

Telemedicine by internist

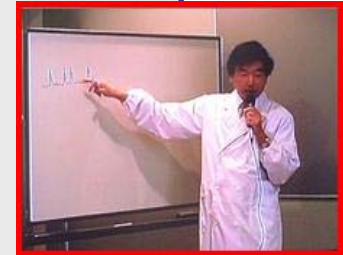


Vision of the Fiber-to-the-Display Project

Medical



Education



家の中まで光がつながる



GI-POF GI型プラスチック光ファイバー

Security



Entertainment





Summary

- The Status of “Photonics Polymer” was reviewed , and the concept of “Fiber to the Display” was proposed.

- We believe that the innovation of giga-bit technologies based on these photonics polymers will bring us back to

“Face-to-Face Communication”.